

# From the *pn* junction to the UFSD design

The role of numerical simulation

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# Summary

## I. Overview of semiconductor devices

- The  $pn$  junction
- Low Gain Avalanche Detectors (LGAD)

## II. Electronic device modeling

- Analytical description
- Numerical implementation

## III. LGAD design using numerical simulations

# Summary

## I. Overview of semiconductor devices

- The *pn* junction
- Low Gain Avalanche Detectors (LGAD)

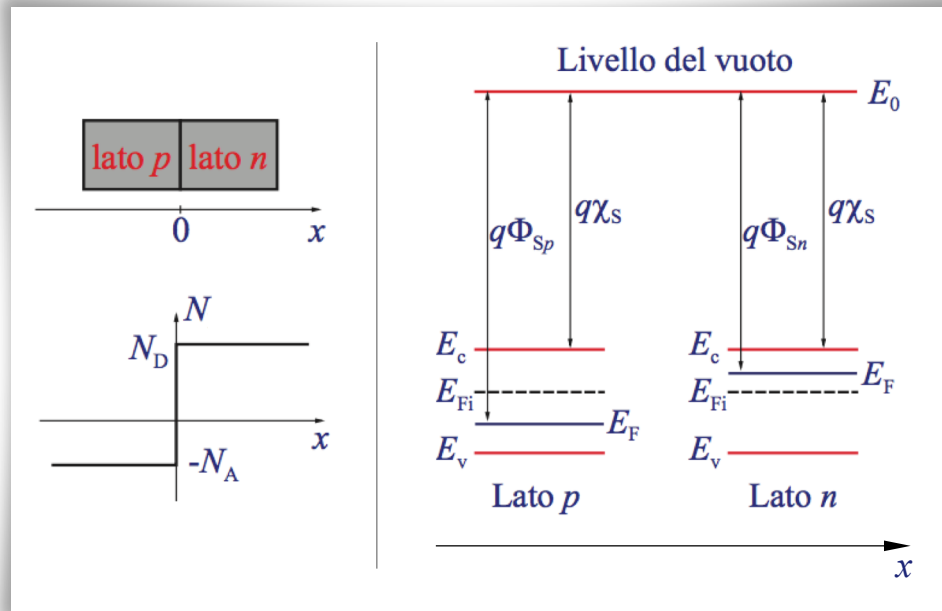
## II. Electronic device modeling

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## III. LGAD design using numerical simulations

# Characteristic equations of the $pn$ junction

- **Definition:** the  $pn$  junction is a semiconductor region where a  $p$ -type and an  $n$ -type doped materials are placed side by side.
- **Example:** the *abrupt junction* of two *uniformly doped* semiconductors.



$q\chi$  is the **electronic affinity** ( $\sim 4.05$  eV in Si)  
 $q\Phi$  is the semiconductor **work function**

$$q\Phi_{Sp} = q\chi_s + E_g - (E_F - E_v) = q\chi_s + E_g - k_B T \ln \frac{N_v}{N_A}$$

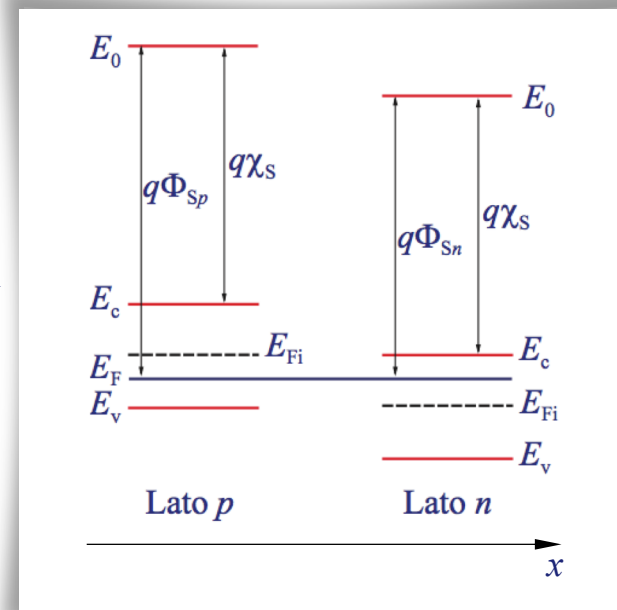
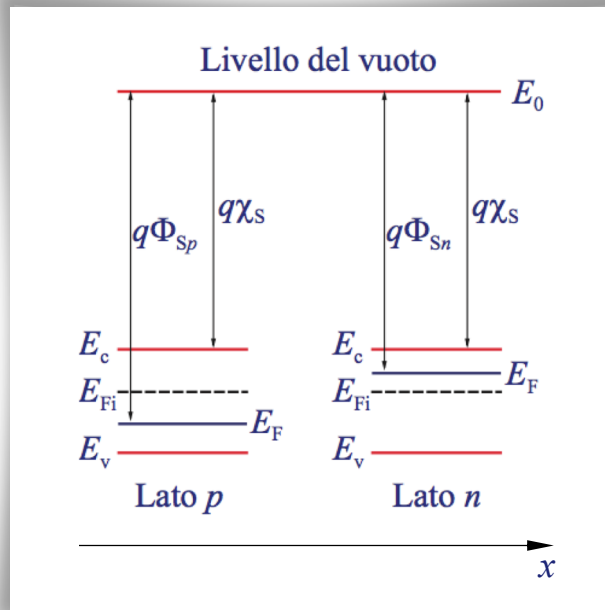
$$q\Phi_{Sn} = q\chi_s + (E_c - E_F) = q\chi_s + k_B T \ln \frac{N_c}{N_D}$$



# Characteristic equations of the $pn$ junction

- Golden-rules to compute the final band-diagram:

- $E_g$  and  $q\chi$  are **conserved** by definition;
- $E_F$  must be **constant** across the junction;



- $E_0$  and bands must be **continuous** functions (in space  $x$ ).

# Characteristic equations of the $pn$ junction

## ► How to fulfill requirement no.3 while still matching 1 and 2?

By introducing the concept of **space-charge region**.

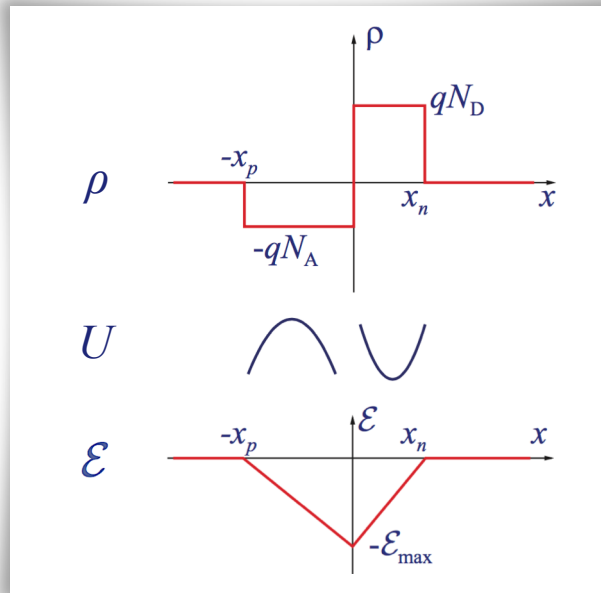
- *Observation #1*: having a **constant  $E_F$**  produces a **transient**, in which **electrons travel from the  $n$ -side to the  $p$ -side** (the vice-versa holds for holes). This mechanism behaves as a **diffusion-like dynamics**.
- *Observation #2*: the **diffusion** of *free* charges **depletes a zone** across the junction, called **space-charge region**.
- *Observation #3*: both in the  **$n$ - and  $p$ -side** of the junction *free* charges are compensated by *fixed* charges of ionized dopants (**neutral regions,  $\rho=0$** ), whereas in the space-charge region this is no more true. So, there,  $\rho \neq 0$ .

# Characteristic equations of the $pn$ junction

- **Within the space-charge region ( $\rho \neq 0$ ) the field is not a constant and bands are no more straight lines.** In particular, due to the **Poisson equation** of semiconductors

$$\frac{d^2U}{dx^2} = q \frac{\rho}{\epsilon}$$

where  $U = -q\phi$  is the *potential energy* felt by free charges, we have



by definition of space-charge region

directly from the Poisson eq.

by 1<sup>st</sup>  $x$ -integration of the Poisson eq.:

$$\frac{d\mathcal{E}}{dx} = \frac{\rho}{\epsilon}$$

# Characteristic equations of the $pn$ junction

- Now consider that, **in neutral regions**,

$$\rho = 0 \implies \frac{d\mathcal{E}}{dx} = 0 \implies \mathcal{E}(x) = \mathcal{E}_0$$

so that **the electrostatic potential**

$$\varphi(x) = -\mathcal{E}_0 x + \varphi_0$$

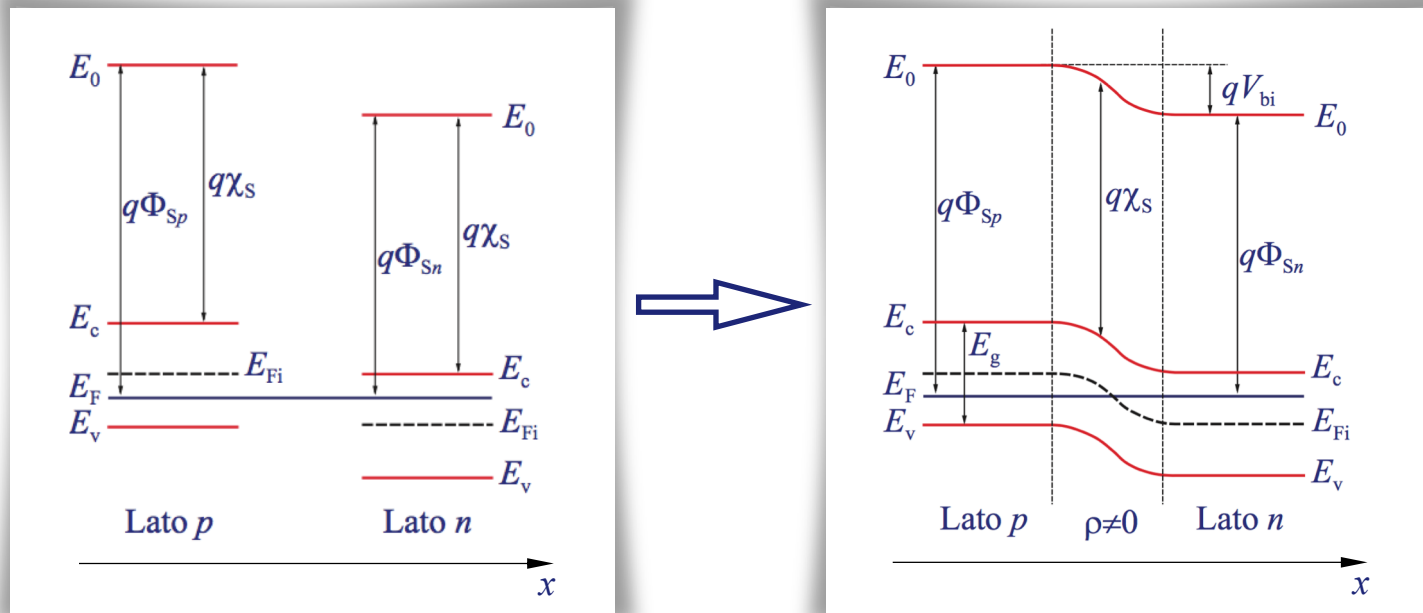
where  $\mathcal{E} = -\frac{\partial\varphi}{\partial x}$ , **is a straight line.**

- If the junction is **at equilibrium** (without any applied bias), then  
and **bands are flat.**

$$\mathcal{E}_0 = 0$$

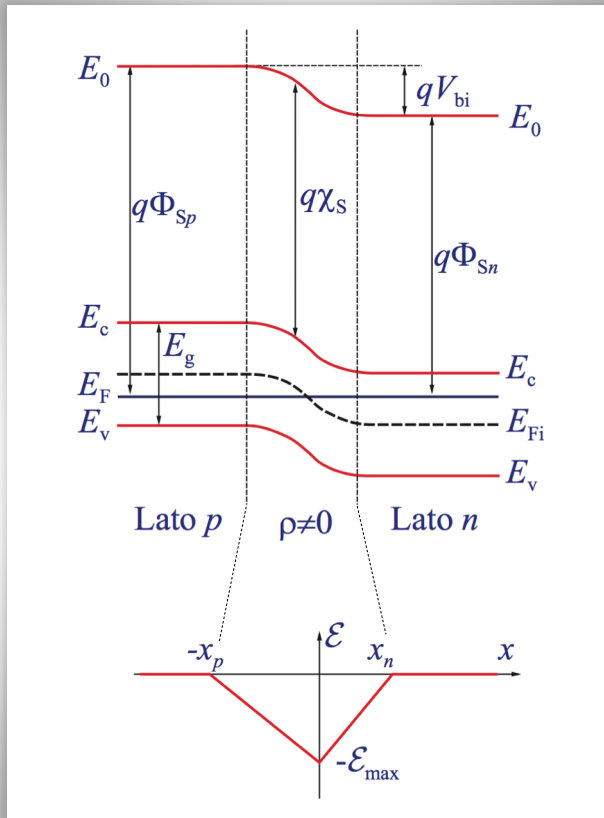
# Characteristic equations of the $pn$ junction

- So, finally we have:



# Characteristic equations of the $pn$ junction

What we concluded has several important physical implications:

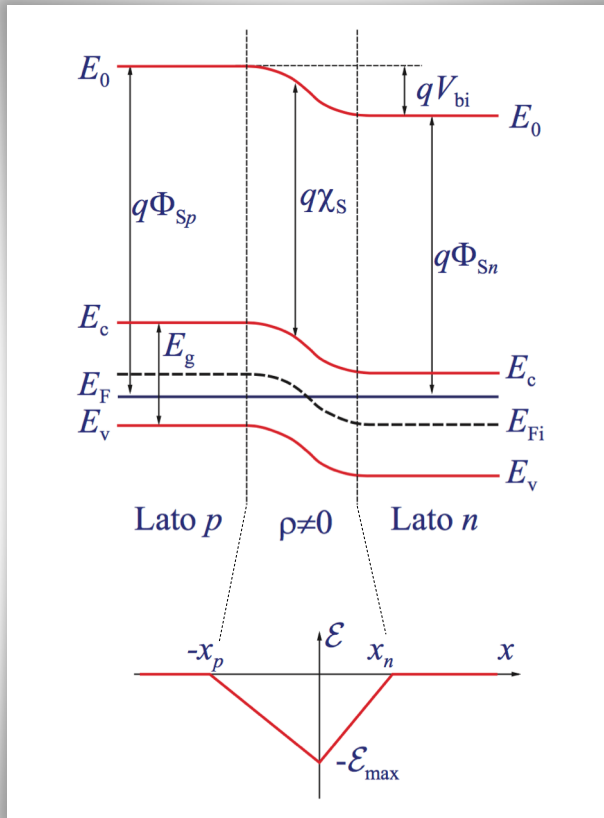


1.  $\mathcal{E} \neq 0$  implies the onset of a **drift current** of carriers tending to **compensate the diffusion** of free charges such that  $J = 0$ ;
2. A **built-in potential**  $qV_{bi}$ , created across the junction, represents an additional **barrier for the diffusion** of electrons towards the  $p$ -side (and holes in the  $n$ -side)

$$\begin{aligned}
 qV_{bi} &= q\Phi_{Sp} - q\Phi_{Sn} = E_g - k_B T \ln \frac{N_v N_c}{N_A N_D} \\
 &= k_B T \ln \frac{N_v N_c}{n_i^2} - k_B T \ln \frac{N_v N_c}{N_A N_D} \\
 &= k_B T \ln \frac{N_A N_D}{n_i^2}
 \end{aligned}$$

# Characteristic equations of the $pn$ junction

What we concluded has several important physical implications:



3. By integrating the Poisson equation, and thanks to the *neutrality law*  $N_A x_p = N_D x_n$ , one has

$$\mathcal{E}(x) = \begin{cases} -\frac{qN_A}{\epsilon}(x + x_p) & -x_p \leq x < 0 \\ \frac{qN_D}{\epsilon}(x - x_n) & 0 \leq x < x_n \end{cases}$$

and

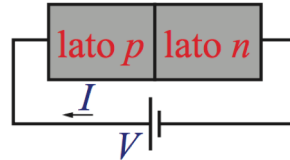
$$\mathcal{E}_{max} = \frac{qN_A}{\epsilon}x_p = \frac{qN_D}{\epsilon}x_n$$

4. In the same way:

$$\varphi(x) = \begin{cases} \frac{qN_A}{2\epsilon}(x + x_p)^2 & -x_p \leq x < 0 \\ -\frac{qN_D}{2\epsilon}(x - x_n)^2 + \frac{qN_A}{2\epsilon}x_p^2 + \frac{qN_D}{2\epsilon}x_n^2 & 0 \leq x < x_n \end{cases}$$

# Characteristic equations of the $pn$ junction

- What happens if the junction is no more at equilibrium?



## Direct polarization

- $V > 0, I > 0$
- $J_{\text{diff}}$  dominates
- electrons from  $n$ - to  $p$ -side
- holes from  $p$ - to  $n$ -side
- $qV < qV_{\text{bi}}$

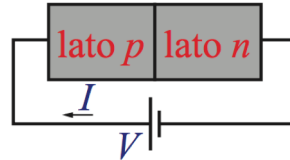
## Reverse polarization

- $V < 0, I < 0$
- $J_{\text{drift}}$  dominates
- electrons from  $p$ - to  $n$ -side
- holes from  $n$ - to  $p$ -side
- $qV > qV_{\text{bi}}$

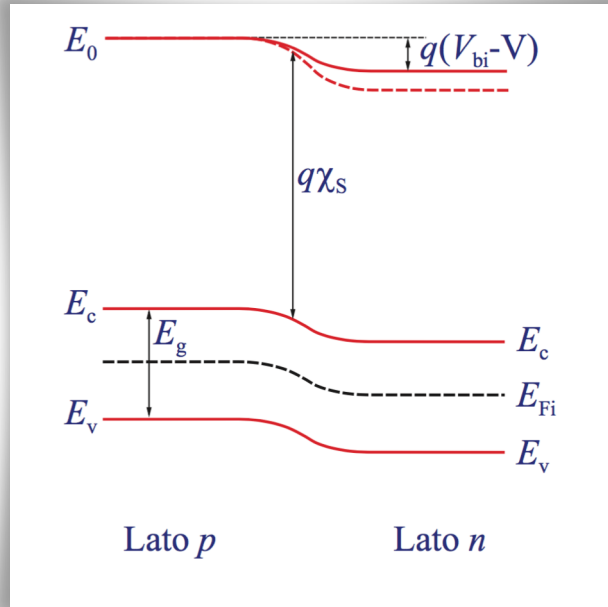


# Characteristic equations of the $pn$ junction

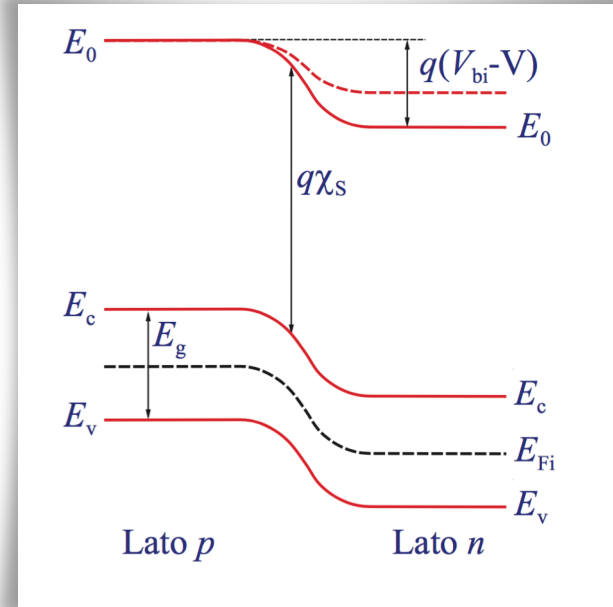
- What happens if the junction is no more at equilibrium?



## Direct polarization



## Reverse polarization



# Characteristic equations of the $pn$ junction

Let's now deduce the static  $I(V)$  **characteristic** of the diode for a 1D structure where  $I = A J$  (with  $A$  its cross-section) is constant at each point  $x$ .

- *Hypothesis #1*: we assume a **null field** and **quasi-equilibrium free charges** in the **neutral regions** of our system. This means that we can **neglect the drift component** of the current for minority charges:

$$\begin{aligned} J &\approx J_{n,\text{diff}}(x) + J_p(x) & x < -x_p \\ J &\approx J_n(x) + J_{p,\text{diff}}(x) & x > x_n \end{aligned}$$

- *Hypothesis #2*: **neutral regions are much longer than the diffusion length**  $L_{n,p}$  (10s to 100s of  $\mu\text{m}$ ) of minority charge carriers.

Being the **diffusion current** driven by the **charge density**, we have to evaluate the **excess densities**  $n'(x)$  and  $p'(x)$  along the whole structure.

# Characteristic equations of the $pn$ junction

In fact:

$$J_{n,\text{diff}} = qD_n \frac{\partial n'}{\partial x}$$
$$J_{p,\text{diff}} = -qD_p \frac{\partial p'}{\partial x}$$

?

with

$$D_n = \frac{kT}{q} \mu_n = V_T \mu_n \quad (\leq 36 \text{ cm}^2/\text{s})$$

$$D_p = \frac{kT}{q} \mu_p = V_T \mu_p \quad (\leq 12 \text{ cm}^2/\text{s})$$

the so-called **Einstein's diffusion coefficients**, and  $\mu$  the electron/hole mobility.

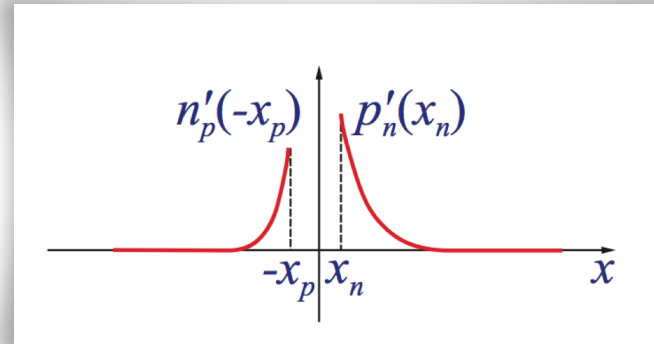
# Characteristic equations of the $pn$ junction

We have:

?

$$n'_p(x) = n'_p(-x_p) \exp\left(\frac{x + x_p}{L_n}\right)$$

$$p'_n(x) = p'_n(x_n) \exp\left(-\frac{x - x_n}{L_p}\right)$$



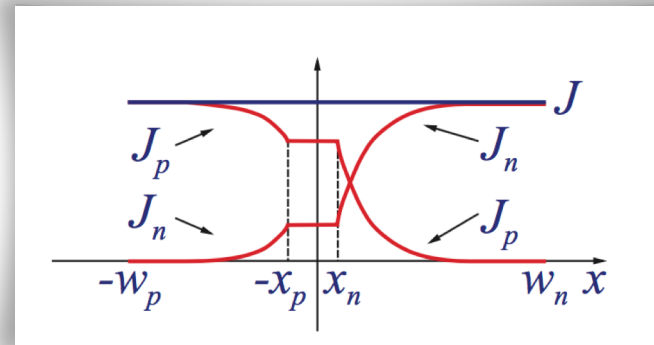
and:

$$J = J_{n,\text{diff}}(-x_p) + J_p(-x_p) = J_n(x_n) + J_{p,\text{diff}}(x_n)$$

$$J_n(x_n) \approx J_{n,\text{diff}}(-x_p) \quad J_p(-x_p) \approx J_{p,\text{diff}}(x_n)$$



$$J \approx J_{n,\text{diff}}(-x_p) + J_{p,\text{diff}}(x_n)$$



# Characteristic equations of the $pn$ junction

Remembering that

$$n'_p = n_p - n_{p0} \quad p'_n = p_n - p_{n0},$$

with

$$n_{n0}(x_n) = N_D \quad n_{p0}(-x_p) = n_i^2/N_A \quad p_{p0}(-x_p) = N_A \quad p_{n0}(x_n) = n_i^2/N_D$$

then

$$V_{bi} = V_T \log \frac{N_A N_D}{n_i^2} = V_T \log \frac{n_{n0}(x_n)}{n_{p0}(-x_p)} = V_T \log \frac{p_{p0}(-x_p)}{p_{n0}(x_n)}$$
$$\frac{p_{n0}(x_n)}{p_{p0}(-x_p)} = \frac{n_{p0}(-x_p)}{n_{n0}(x_n)} = \exp\left(-\frac{V_{bi}}{V_T}\right)$$

# Characteristic equations of the $pn$ junction

Rewriting

$$\frac{p_{n0}(x_n)}{p_{p0}(-x_p)} = \frac{n_{p0}(-x_p)}{n_{n0}(x_n)} = \exp\left(-\frac{V_{bi}}{V_T}\right)$$

in the *low-injection regime*

$$\frac{p_n(x_n)}{p_p(-x_p)} \approx \frac{n_p(-x_p)}{n_n(x_n)} \approx \exp\left(-\frac{V_{bi} - V}{V_T}\right)$$

and assuming

$$n_n(x_n) \approx n_{n0}(x_n) = N_D \quad p_p(-x_p) \approx p_{p0}(-x_p) = N_A$$

we have the **junction law**

$$n_p(-x_p) = n_{p0}(-x_p) \exp\left(\frac{V}{V_T}\right) \quad p_n(x_n) = p_{n0}(x_n) \exp\left(\frac{V}{V_T}\right)$$

so that

$$\frac{n'_p(-x_p)}{n_{p0}(-x_p)} = \exp\left(\frac{V}{V_T}\right) - 1 \quad \frac{p'_n(x_n)}{p_{n0}(x_n)} = \exp\left(\frac{V}{V_T}\right) - 1$$

# Characteristic equations of the $pn$ junction

Now, by plugging the junction law into the current densities

$$\begin{aligned}
 p_n(x_n) &= \frac{n_i^2}{N_D} \exp\left(\frac{V}{V_T}\right) & J_{n,\text{diff}} &= qD_n \frac{\partial n'}{\partial x} \\
 n_p(-x_p) &= \frac{n_i^2}{N_A} \exp\left(\frac{V}{V_T}\right) & J_{p,\text{diff}} &= -qD_p \frac{\partial p'}{\partial x}
 \end{aligned}
 \Rightarrow$$

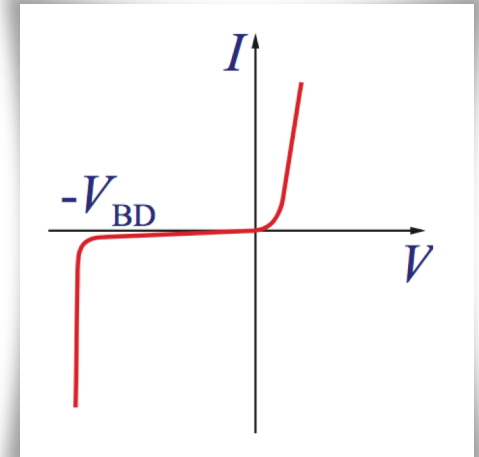
one finds

$$J_{n,\text{diff}}(-x_p) = qD_n \frac{n_p'(-x_p)}{L_n}$$

$$J_{p,\text{diff}}(x_n) = qD_p \frac{p_n'(x_n)}{L_p}$$

and we end up with the expression

$$I = qA \frac{n_i^2}{N_A} \frac{D_n}{L_n} + qA \frac{n_i^2}{N_D} \frac{D_p}{L_p} \left[ \exp\left(\frac{V}{V_T}\right) - 1 \right]$$



# Summary

## I. Overview of semiconductor devices

- The *pn* junction
- **Low Gain Avalanche Detectors (LGAD)**

## II. Electronic device modeling

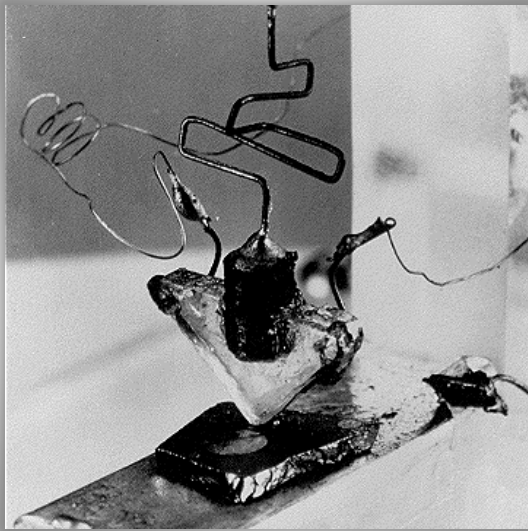
- Analytical description
- Numerical implementation

## III. LGAD design using numerical simulations



# Towards a technological step...

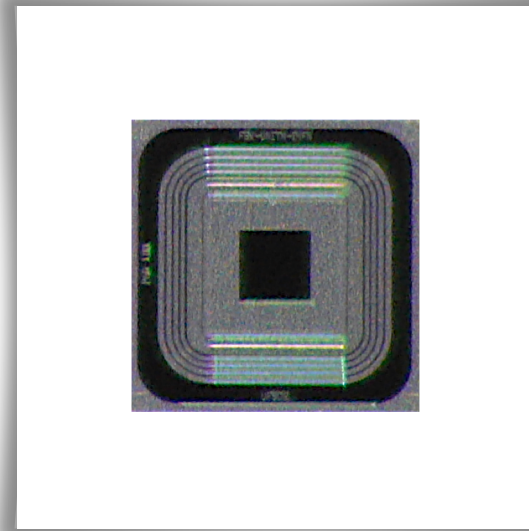
first *n-p-n* “tip”-transistor



J. Bardeen, W. Brattain, W. Shockley  
Bell Labs. - NJ  
(1948)



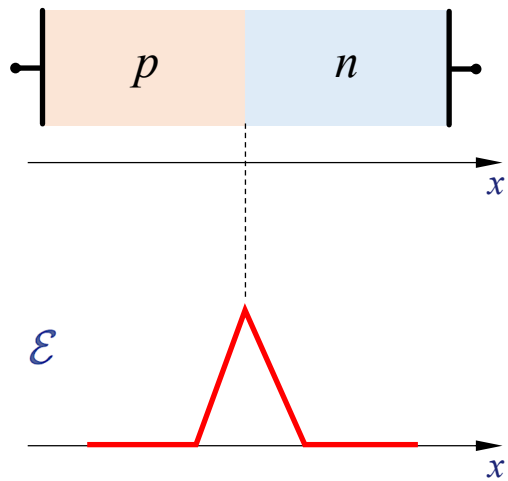
Ultra Fast Silicon Detector



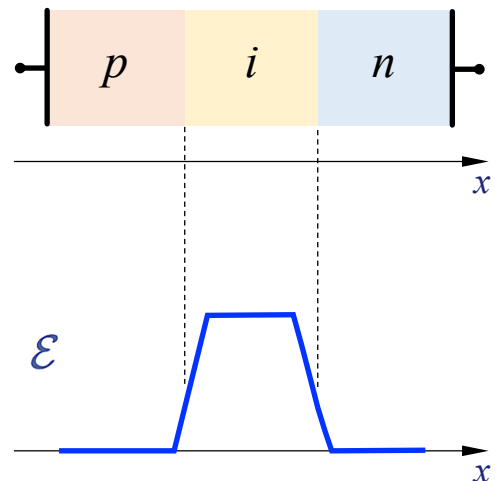
UFSD Group  
INFN Torino and FBK Trento  
(2018)

# Extending our application domain to other systems

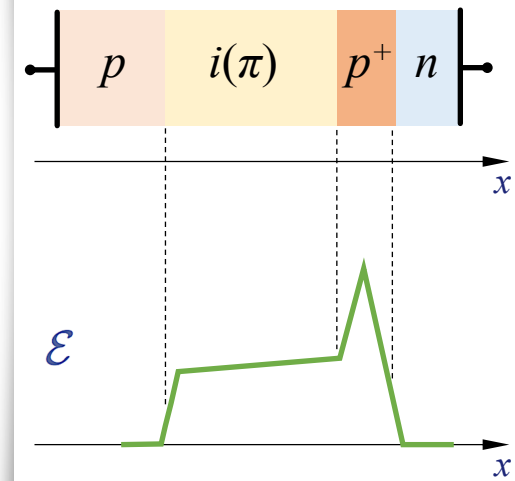
***pn junction***



***pin diode***

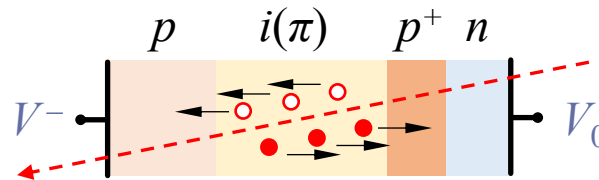


**LGAD**



# Working principles of an LGAD

## ► What is charge multiplication in LGAD?



- **Primary charges** (electron/hole pairs) are produced by **ionization**, while the particle is crossing the sensor;
- Due to the **reverse field**, electrons **drift** towards the  $n$ -side and holes towards the  $p$ -side;
- When electrons travel along the  $p^+$  **region** (the *gain-* or *multiplication-*layer) they experience an **high field**;
- This field is responsible for the **impact ionization**, which produces an avalanche **multiplication of secondary charges**;
- Now the **total current** is due to the **additional avalanche contribution**.

# Working principles of an LGAD

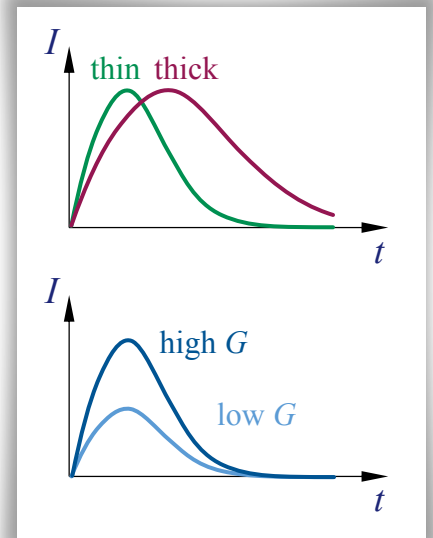
## ► Why using LGAD to detect particles at CERN?

### I. We need **charge multiplication**:

1. LGAD exploit the so-called **avalanche multiplication**, a process which belongs to the class of **generation/recombination (GR) mechanisms**;
2. Charge multiplication allows to obtain **large and fast signals**:
  - the **thinner** the sensor, the **faster** the signal;
  - the **higher** the **gain**, the **larger** the signal.

### II. We need a good **S/N**:

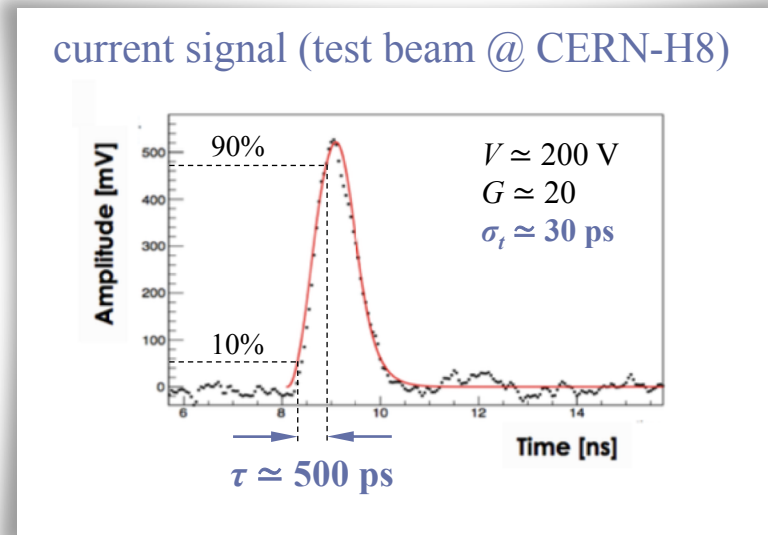
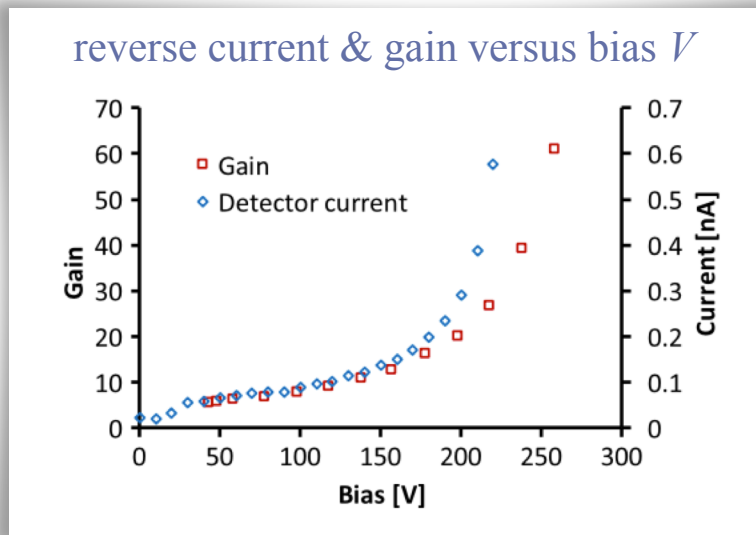
1. Also the **noise** related to the current signal is **proportional to the gain**
2. The **gain  $G$**  has to be kept as **low** as required by electronics ( $G \sim 10-20$ )



# Working principles of an LGAD

## ► Why using LGAD to detect particles at CERN?

Examples of 50  $\mu\text{m}$  LGAD performance:



# Working principles of an LGAD

## ► Can we predict the avalanche contribution to the total current?

Let's introduce a bit of physical-mathematics...

1. The **avalanche** process is modeled via its **ionization coefficient**  $\alpha$ , i.e. the **inverse of the electron/hole mean free path** ( $\text{cm}^{-1}$ );
2. In the literature, several **expressions of  $\alpha$**  are available. In general, all of them are based on the **Chynoweth's theory** (1958), according to which:

$$\alpha_{n,p}(\mathcal{E}) = \gamma A_{n,p} \exp\left(-\gamma \frac{B_{n,p}}{\mathcal{E}}\right)$$

3. Once the coefficient has been obtained, one has to evaluate the **net avalanche generation rate**  $U_{\text{aval}}$ , i.e. the **number of multiplied e<sup>-</sup>/h<sup>+</sup> pairs per volume** ( $\text{cm}^{-3}$ ) **per unit time** ( $\text{s}^{-1}$ ), as:

$$U_{\text{aval}} = \frac{dn}{dt} = \frac{dp}{dt} = \alpha_n n v_n + \alpha_p p v_p$$

... Now we need a complete description of the system!

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# Electronic device modeling - I

- We recall the **twofold nature of the current** in a semiconductor device:
  - Drift current**, driven by the *electric field*;
  - Diffusion current**, due to the density gradient of *free charges*.

$$J_{n,\text{dr}} = qn\mu_n\mathcal{E} \quad J_{p,\text{dr}} = qp\mu_p\mathcal{E}$$

$$J_{n,\text{diff}} = qD_n\frac{\partial n}{\partial x} \quad J_{p,\text{diff}} = -qD_p\frac{\partial p}{\partial x}$$

$$J = \underbrace{J_{n,\text{diff}} + J_{n,\text{dr}}}_{J_n} + \underbrace{J_{p,\text{diff}} + J_{p,\text{dr}}}_{J_p}$$

- Then we introduce (all) the **GR mechanisms** through their **net rates  $U$** :

$$U_n = R_n - G_n \\ \approx \frac{n - n_0}{\tau_n} = \frac{n'}{\tau_n}$$

$$U_p = R_p - G_p \\ \approx \frac{p - p_0}{\tau_p} = \frac{p'}{\tau_p}$$

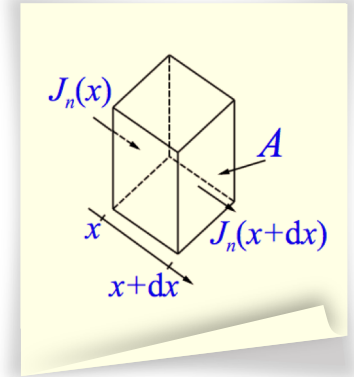


# Electronic device modeling - I

- To derive the **global current density** (field + charge + GR):

1. in a volume  $dV = A dx$  the **time variation of the electron density** (similarly for holes) is

$$\frac{\partial n}{\partial t} A dx = \underbrace{\frac{J_n(x)}{-q} A - \frac{J_n(x + dx)}{-q} A}_{\text{field + charge}} + \underbrace{G_n A dx - R_n A dx}_{\text{GR}}$$



2. by using the 1<sup>st</sup>-order Taylor series expansion

$$J_n(x + dx) \approx J_n(x) + \frac{\partial J_n}{\partial x} dx$$

and assuming  $dx \rightarrow 0$ , we obtain the **continuity equations**:

$$\frac{\partial n}{\partial t} = \frac{1}{q} \frac{\partial J_n}{\partial x} - U_n \quad \frac{\partial p}{\partial t} = -\frac{1}{q} \frac{\partial J_p}{\partial x} - U_p$$

# Electronic device modeling - I

- Since the drift component depends on the **electric field**, we need a third equation to close the system, the **Poisson equation**, which connects the *field* to the *charge densities*.

The final (1D) mathematical framework is:

$$\begin{array}{l}
 \text{continuity eqs.} \rightarrow \left\{ \begin{array}{l} \frac{\partial n}{\partial t} = \frac{1}{q} \frac{\partial J_n}{\partial x} - U_n \\ \frac{\partial p}{\partial t} = -\frac{1}{q} \frac{\partial J_p}{\partial x} - U_p \end{array} \right. \\
 \text{Poisson eq.} \rightarrow \left\{ \begin{array}{l} \frac{\partial \mathcal{E}}{\partial x} = \frac{\rho}{\epsilon} \end{array} \right.
 \end{array}$$

**DRIFT-DIFFUSION  
MODEL (DD)**

where  $J_n = q\mu_n n \mathcal{E} + qD_n \frac{\partial n}{\partial x}$ ,  $J_p = q\mu_p p \mathcal{E} - qD_p \frac{\partial p}{\partial x}$

**TRANSPORT EQS.**

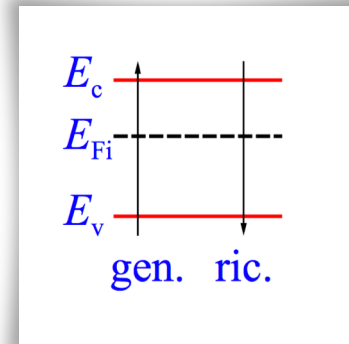
and  $\mathcal{E} = -\frac{\partial \varphi}{\partial x}$ ,  $\rho = q(p - n + N_D^+ - N_A^-)$ .

# Electronic device modeling - I

- Avalanche generation is not the only **GR mechanism** occurring in silicon devices. In general, we have to account for **two different families**:

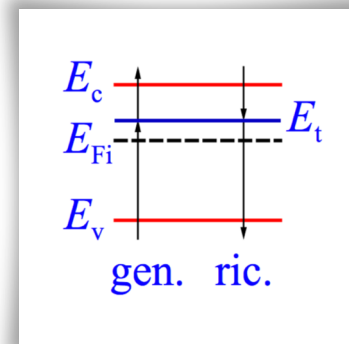
## A. **Band-to-band** generation/recombination

- *Auger*
- *direct tunneling*
- ...



## B. **Defect-assisted** generation/recombination

- *Shockley-Read-Hall (SRH)*
- *trap-assisted tunneling*
- ...



# Electronic device modeling - I

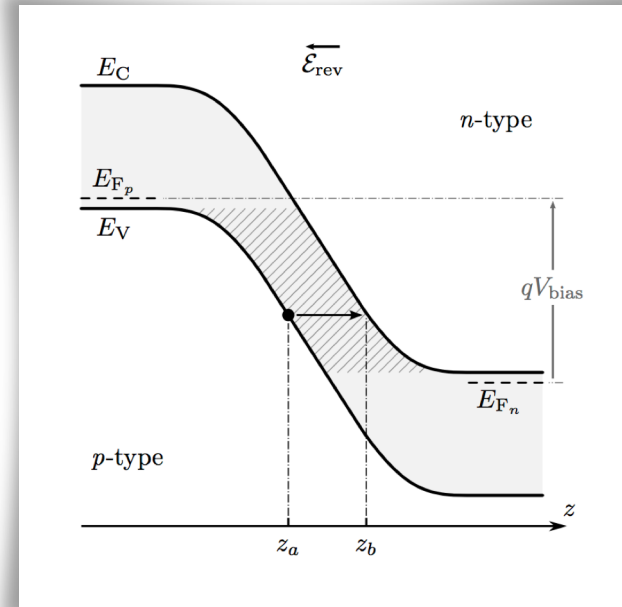
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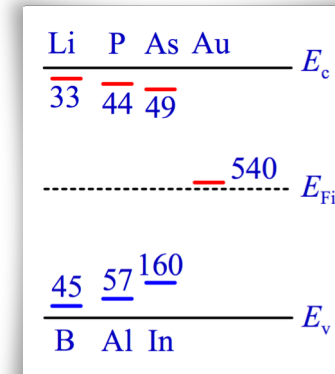
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## A. **Band-to-band** generation/recombination

- *Auger*
- *direct tunneling*
- ...

## B. **Defect-assisted** generation/recombination

- *Shockley-Read-Hall (SRH)*
- *trap-assisted tunneling*
- ...



# Electronic device modeling - I

- **SRH** processes are determined by such a net rate statistics

$$U_{\text{SRH}} = \frac{np - n_i^2}{\tau_p \left( n + n_i e^{\frac{E_{\text{trap}} - E_{\text{F}_i}}{k_B T}} \right) + \tau_n \left( p + n_i e^{\frac{E_{\text{F}_i} - E_{\text{trap}}}{k_B T}} \right)}$$

where  $\tau_{n,p}$  are proper **electron/hole lifetimes**, i.e. the average time interval ( $\sim 10^{-7}$ - $10^{-9}$  s) between two consecutive scattering processes originating (or annihilating)  $e^-/h^+$  pairs.

- Moreover, **band-to-band tunneling** is modeled with the usual Kane expression (1961)

$$U_{\text{tunn}} = A \mathcal{E}^2 \cdot \exp(-B/\mathcal{E})$$

with  $A$  and  $B$  (V/cm) material-dependent parameters.

# Summary

## I. Overview of semiconductor devices

- The  $pn$  junction
- Low Gain Avalanche Detectors (LGAD)

## II. Electronic device modeling

- Analytical description
- Numerical implementation

## III. LGAD design using numerical simulations

# Electronic device modeling - II

- We need a method to compute the DD model

$$\left\{ \begin{array}{l} \frac{\partial n}{\partial t} = \frac{1}{q} \frac{\partial J_n}{\partial x} - U_n \\ \frac{\partial p}{\partial t} = -\frac{1}{q} \frac{\partial J_p}{\partial x} - U_p \\ \frac{\partial \mathcal{E}}{\partial x} = \frac{\rho}{\epsilon} \end{array} \right.$$

where  $\varphi$  is the input function,  $n$ ,  $p$  and  $\mathcal{E}$  are the unknowns of the continuity equations and where the Poisson equation closes the system.

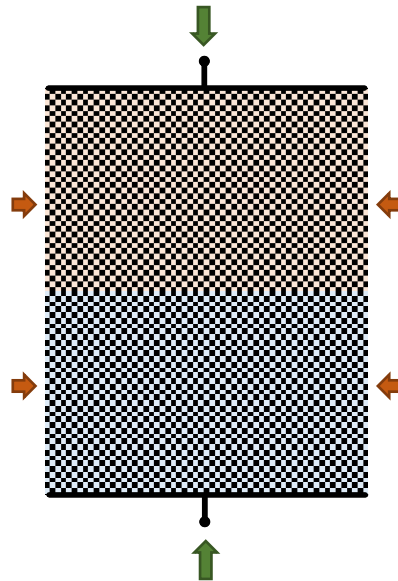
- We have to solve a set of *non-linear, secondary-order PDEs, in space and time, for the whole device!*



# Electronic device modeling - II

## ▪ The strategy

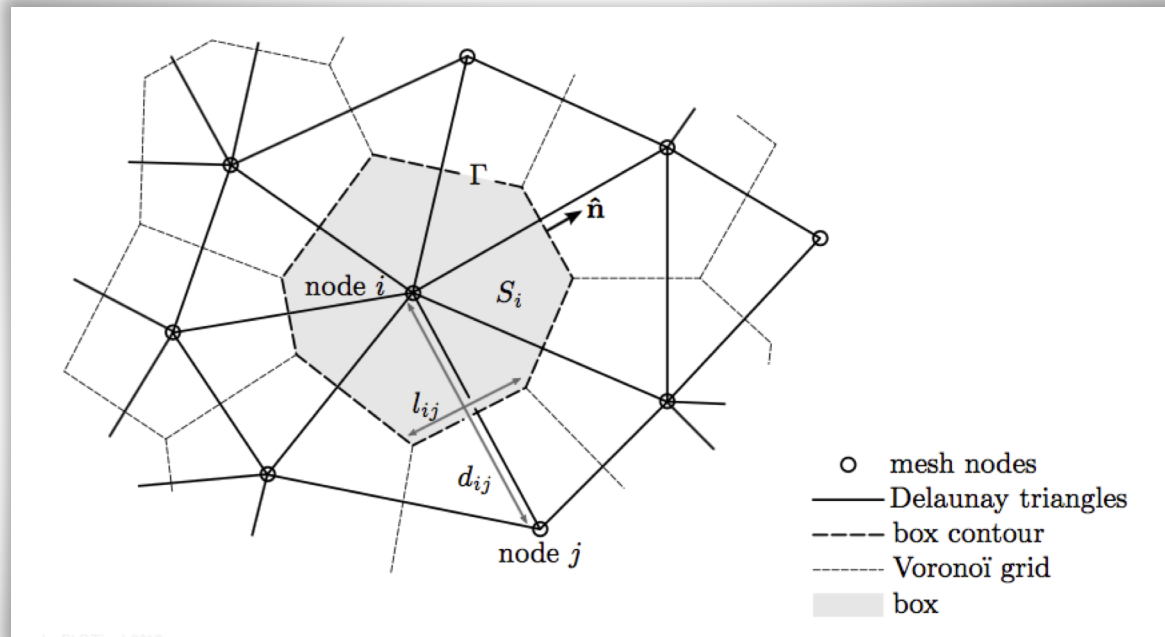
- Dynamics (bias ramps, transients, ...) is treated as a sequence of *small increments between stationary states at equilibrium*: the **quasi-stationary process**;
- At each quasi-stationary step the mathematics has to be **simplified** through proper **approximations** and **algorithms**:



1. the **geometry** is **discretized** (e.g.: Delaunay-Voronoi procedure)
2. DD system is rewritten and adapted to the mesh grid
3. PDEs are linearized and transformed into **ODEs (FD schemes)**
4. **I.C.** and **B.C.** are defined
5. the *new* DD model is solved via **iterative methods** (Newton) in all mesh nodes

# Electronic device modeling - II

## 1. The geometry is discretized (e.g.: Delaunay-Voronoi procedure)



design of **nodes**

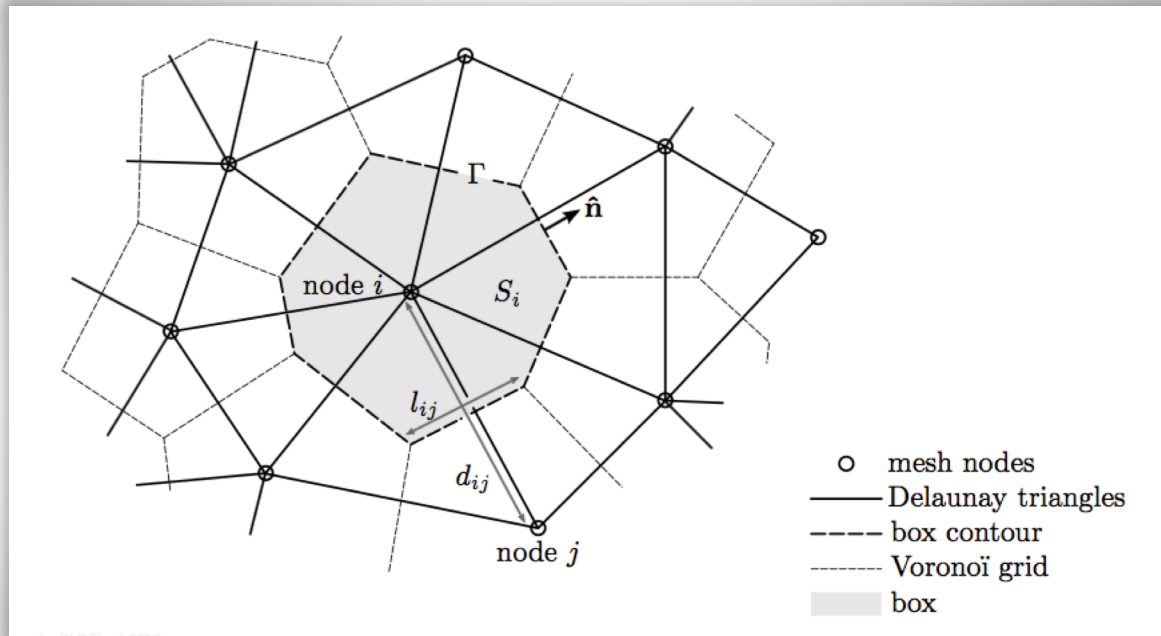
creation of  
**non-obtuse triangles**

creation of **boxes**

$\mathbf{J}_{\perp n,p}$  are conserved  
at boxes interfaces

# Electronic device modeling - II

## 2. Drift-Diffusion system is rewritten and adapted to the mesh grid



scalar/vector operators  
 and constants are  
 transformed:

$$\frac{\partial}{\partial t} \int_S x \, ds \Rightarrow \frac{\partial x_i}{\partial t} S_i$$

$$\oint_{\Gamma} \mathbf{F}_{\perp} \, d\gamma \Rightarrow \sum_j l_{ij} \langle \mathbf{F}_{\perp} \rangle_{ij}$$

$$\int_S c \, ds \Rightarrow c_i S_i$$

by averaging the  
**in/out quantities** at  
 each box side, they are  
 computed at **nodes**

# Electronic device modeling - II

## 3. PDEs are linearized and transformed into ODEs (FD schemes)

FD central differences + Scharfetter-Gummel scheme

$$\frac{\partial n}{\partial t} = \frac{1}{q} \frac{\partial J_n}{\partial x} - U_n$$

$$\frac{\partial p}{\partial t} = -\frac{1}{q} \frac{\partial J_p}{\partial x} - U_p$$

$$\frac{\partial \mathcal{E}}{\partial x} = \frac{\rho}{\epsilon}$$



$$\langle \mathcal{E}_\perp \rangle_{ij} = -\frac{\partial \phi_{ij}(\mathbf{r}, t)}{\partial \mathbf{r}} \approx \frac{\phi_i(\mathbf{r}, t) - \phi_j(\mathbf{r}, t)}{d_{ij}}$$

$$\frac{1}{q} \langle \mathbf{J}_{\perp n} \rangle_{ij} \approx \frac{1}{q} \nabla \mathbf{J}_{\perp n}$$

$$= -\mu_n n(\mathbf{r}) \frac{\partial \phi_{ij}(\mathbf{r}, t)}{\partial \mathbf{r}} + D_n \frac{dn(\mathbf{r}, t)}{d\mathbf{r}}$$

$$\approx -\mu_n n(\mathbf{r}, t) \frac{\phi_i(\mathbf{r}) - \phi_j(\mathbf{r}, t)}{d_{ij}} + D_n \frac{dn(\mathbf{r}, t)}{d\mathbf{r}}$$

$$\stackrel{\text{SG}}{\approx} \frac{D_n}{d_{ij}} [n_j(\mathbf{r}, t) \mathbf{B}(\Delta_{ij}) - n_i(\mathbf{r}, t) \mathbf{B}(-\Delta_{ij})]$$

with:

$$\Delta_{ij} = q \frac{\phi_i(\mathbf{r}, t) - \phi_j(\mathbf{r}, t)}{k_B T} = \frac{\phi_i(\mathbf{r}, t) - \phi_j(\mathbf{r}, t)}{V_T}$$

and

$$\mathbf{B}(\alpha) = \frac{\alpha}{e^\alpha - 1}$$



$$\frac{\partial n_i(\mathbf{r}, t)}{\partial t} = \sum_j \frac{D_n l_{ij}}{d_{ij} S_i} [n_j(\mathbf{r}, t) \mathbf{B}(\Delta_{ij}) - n_i(\mathbf{r}, t) \mathbf{B}(-\Delta_{ij})] - U_{n,i}(\mathbf{r}, t)$$

$$\frac{\partial p_i(\mathbf{r}, t)}{\partial t} = -\sum_j \frac{D_p l_{ij}}{d_{ij} S_i} [p_i(\mathbf{r}, t) \mathbf{B}(\Delta_{ij}) - p_j(\mathbf{r}, t) \mathbf{B}(-\Delta_{ij})] - U_{p,i}(\mathbf{r}, t)$$

$$\frac{\partial \mathcal{E}}{\partial x} = \sum_j l_{ij} \langle \mathcal{E}_\perp \rangle_{ij}$$

$$\approx \sum_j l_{ij} \frac{\phi_i(\mathbf{r}, t) - \phi_j(\mathbf{r}, t)}{d_{ij}}$$

# Electronic device modeling - II

## 4. I.C. and B.C. are defined

**Initial Conditions:** starting polarization at contacts

**Boundary Conditions:**

$$\frac{\partial n(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} = 0, \quad \frac{\partial p(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} = 0 \quad \text{and} \quad \frac{\partial \phi(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} = 0 \quad \text{Neumann homogeneous (insulators, external edges,...)}$$

$$\begin{cases} n(\mathbf{r}, t) \mu_n \frac{\partial \phi(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} = D_n \frac{\partial n(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} \\ p(\mathbf{r}, t) \mu_p \frac{\partial \phi(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} = -D_p \frac{\partial p(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} \\ \epsilon_s \frac{\partial \phi(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} \Big|_s = \epsilon_{\text{diel}} \frac{\partial \phi(\mathbf{r}, t)}{\partial \hat{\mathbf{n}}} \Big|_{\text{diel}} \end{cases} \quad \text{Neumann non-homogeneous (dielectrics)}$$

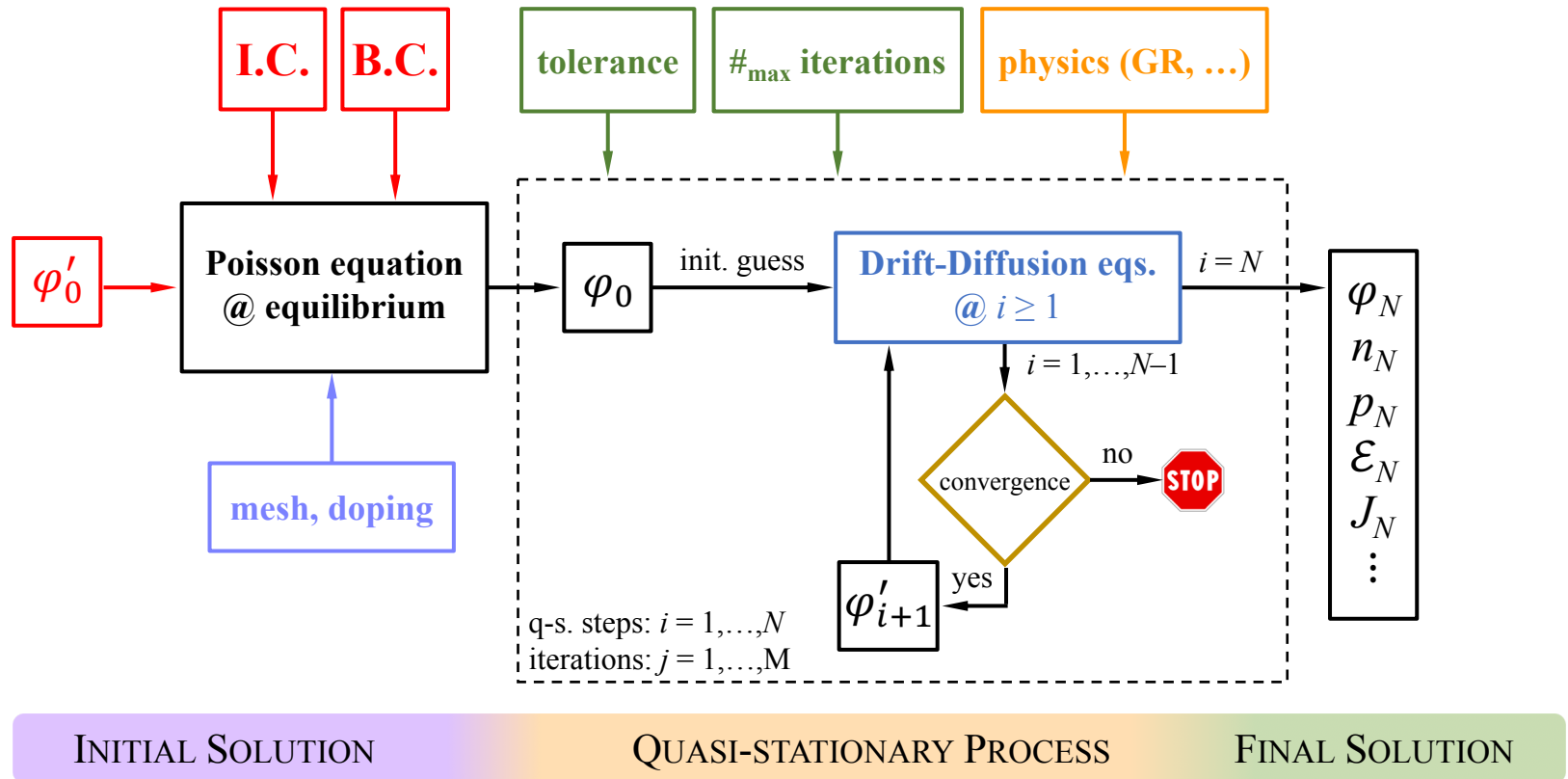
$$\begin{cases} n(\mathbf{r}, t) = \frac{1}{2} \left( \sqrt{\sum_k C_k^{\pm 2}(\mathbf{r}, t) + 4n_i^2} + \sum_k C_k^{\pm}(\mathbf{r}, t) \right) \\ p(\mathbf{r}, t) = \frac{1}{2} \left( \sqrt{\sum_k C_k^{\pm 2}(\mathbf{r}, t) + 4n_i^2} - \sum_k C_k^{\pm}(\mathbf{r}, t) \right) \\ \phi(t) = V_{\text{bias}}(t) + \text{const.} \end{cases} \quad \text{Dirichlet non-homogeneous (contacts)}$$

# Electronic device modeling - II

5. the *new* DD model is solved via **iterative methods** (Newton) in all mesh nodes
- a. Find an **initial guess** for the potential;
  - b. Choose a **maximum number of iterations** and a **tolerance** (max. difference between the solution and our guess);
  - c. The **initial solution** (at equilibrium) is obtained by **solving only the Poisson equation** using the **I.C.** and **B.C.**;
  - d. If we perform a **bias ramp**, or a transient, each step of the ramp is treated as a **quasi-stationary state**. The Poisson solution is used as initial guess for solving the **continuity equations** at step  $i = 1$ ;
  - e. At each state, the **solution** is a function of the **previous two steps**, if available (*Newton-Raphson scheme*):
    - If the **solution** is found **within the maximum number of iterations** and with an **error less than the tolerance**, then **the system converges** and the scheme go further, otherwise the method is aborted;
    - The **self-consistent solution** of the **Poisson-continuity equations** (DD) at steps  $i \geq 1$  proceeds with the same scheme until the end of the ramp.

# Electronic device modeling - II

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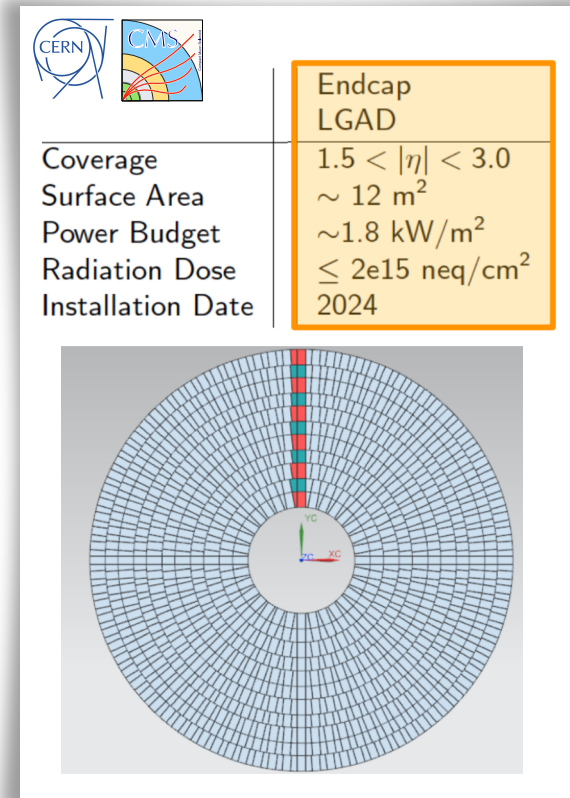
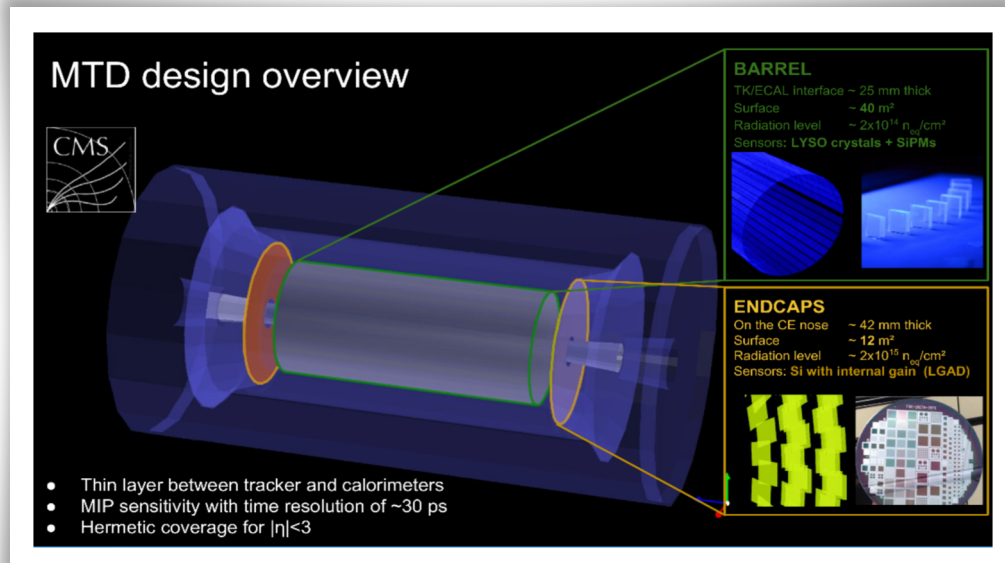
## III. LGAD design using numerical simulations



# Design and simulation of LGAD

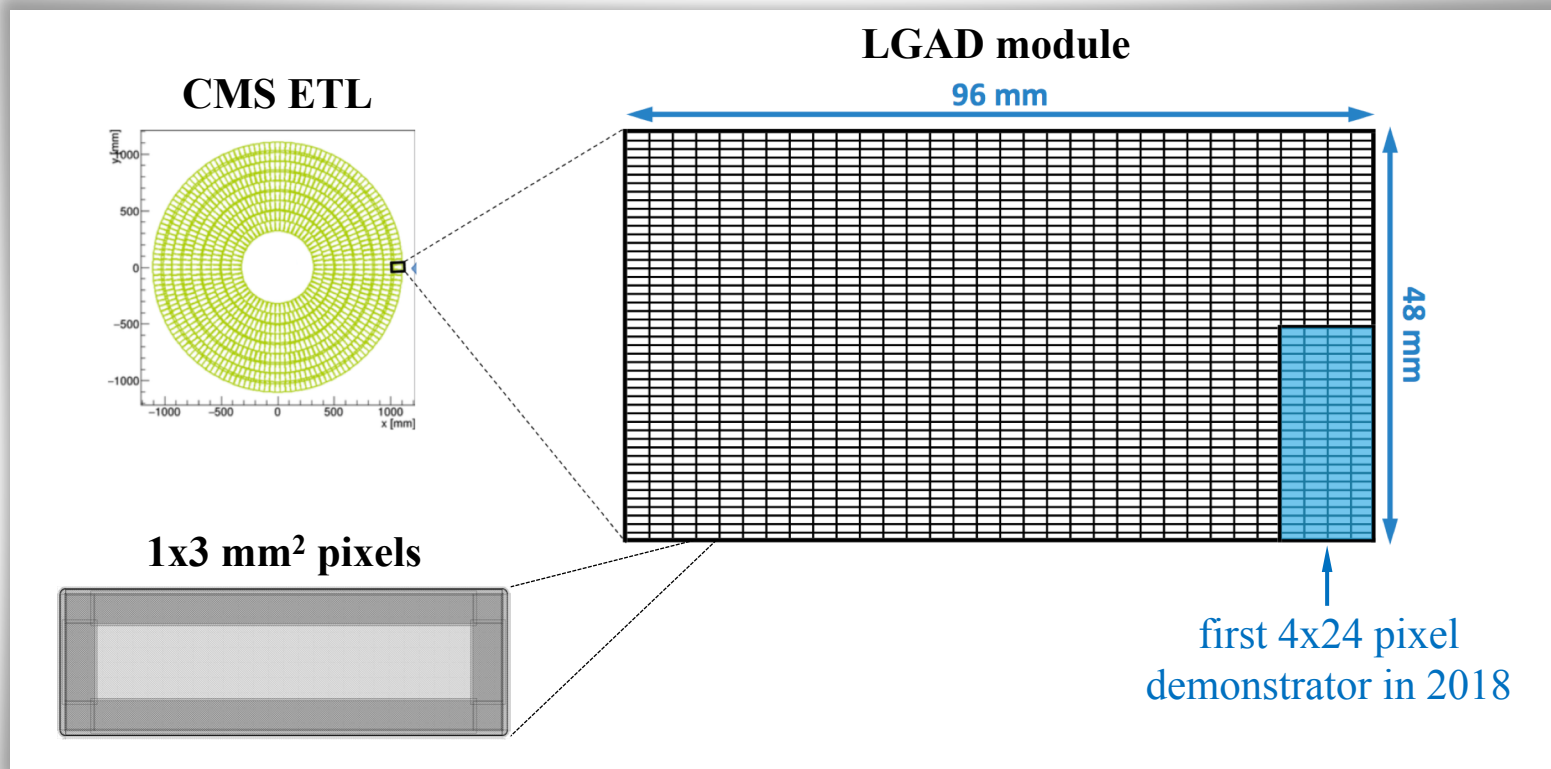
## ► Why LGAD are so innovative?

- Large signals coupled with low Gain  $\Rightarrow$  **high S/N**
- Fast signals  $\Rightarrow$  **high time resolution**
- Simple design  $\Rightarrow$  **low production cost**
- Huge ongoing R&D  $\Rightarrow$  **radiation hardness**



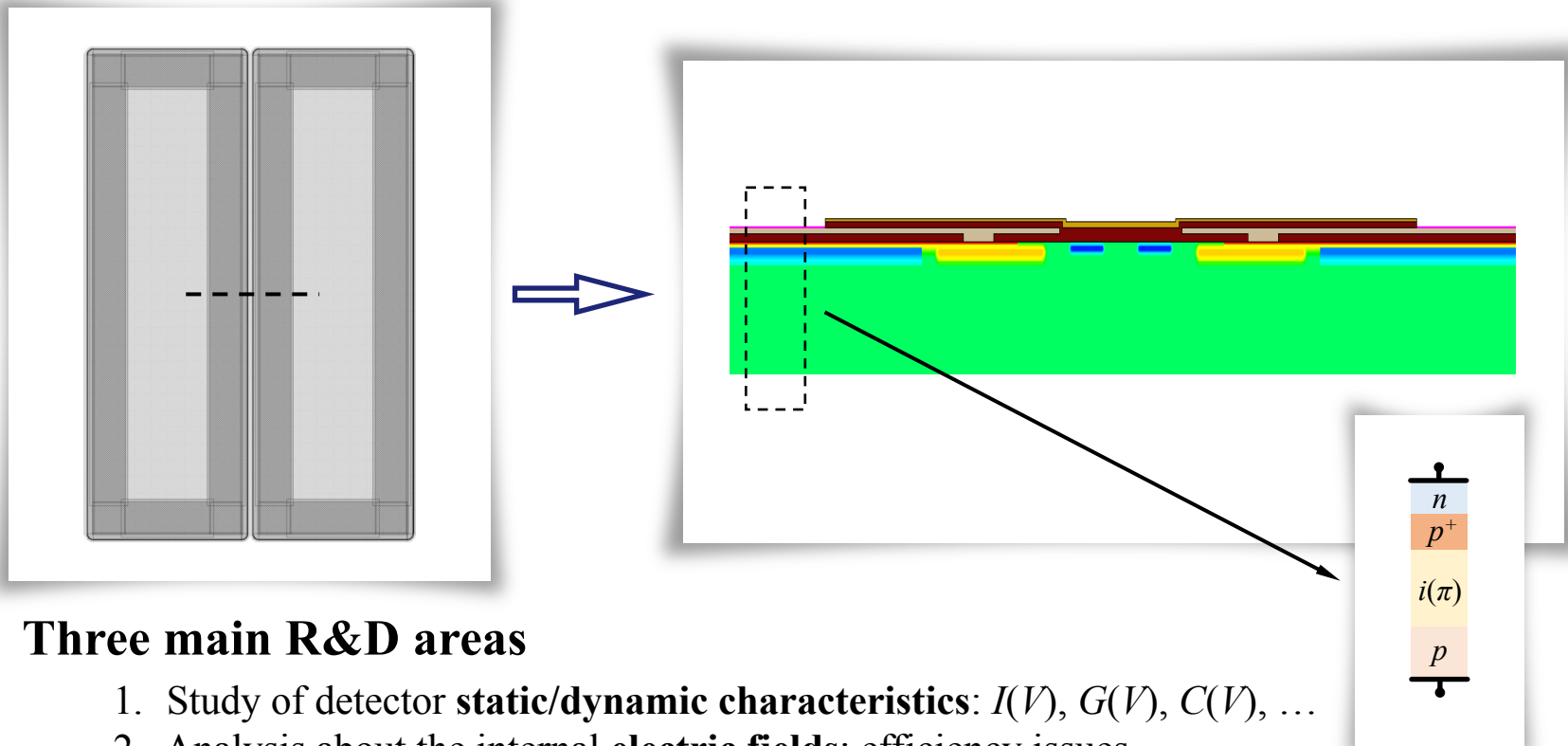
# Design and simulation of LGAD

- How a real LGAD module is made?



# Design and simulation of LGAD

## ► How a real LGAD module is made?

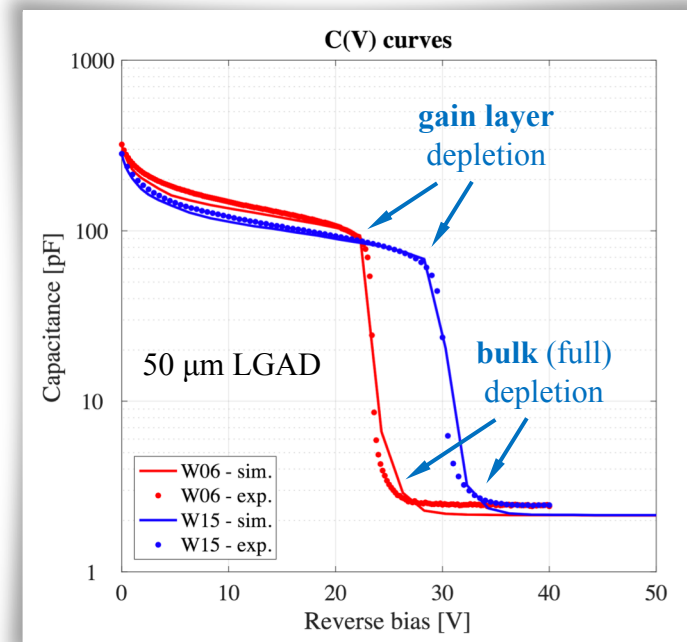
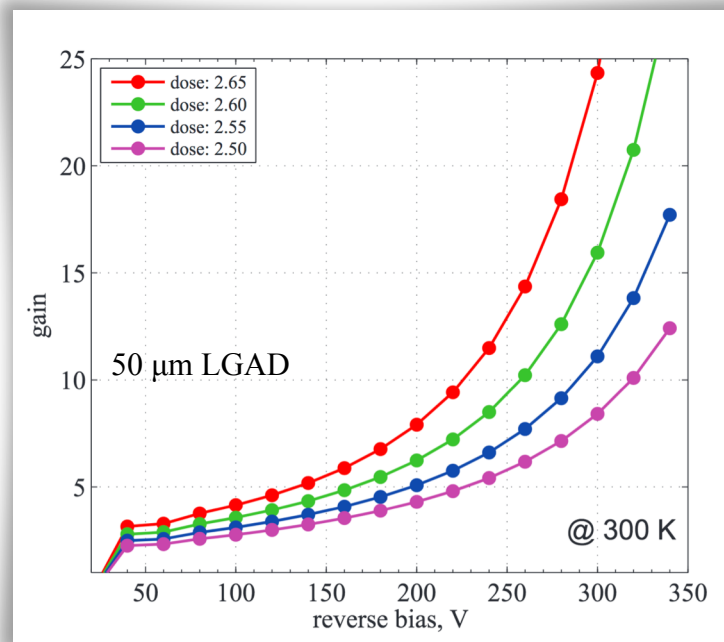


## Three main R&D areas

1. Study of detector **static/dynamic characteristics**:  $I(V)$ ,  $G(V)$ ,  $C(V)$ , ...
2. Analysis about the internal **electric fields**: efficiency issues, ...
3. **Radiation tolerance**

# Design and simulation of LGAD

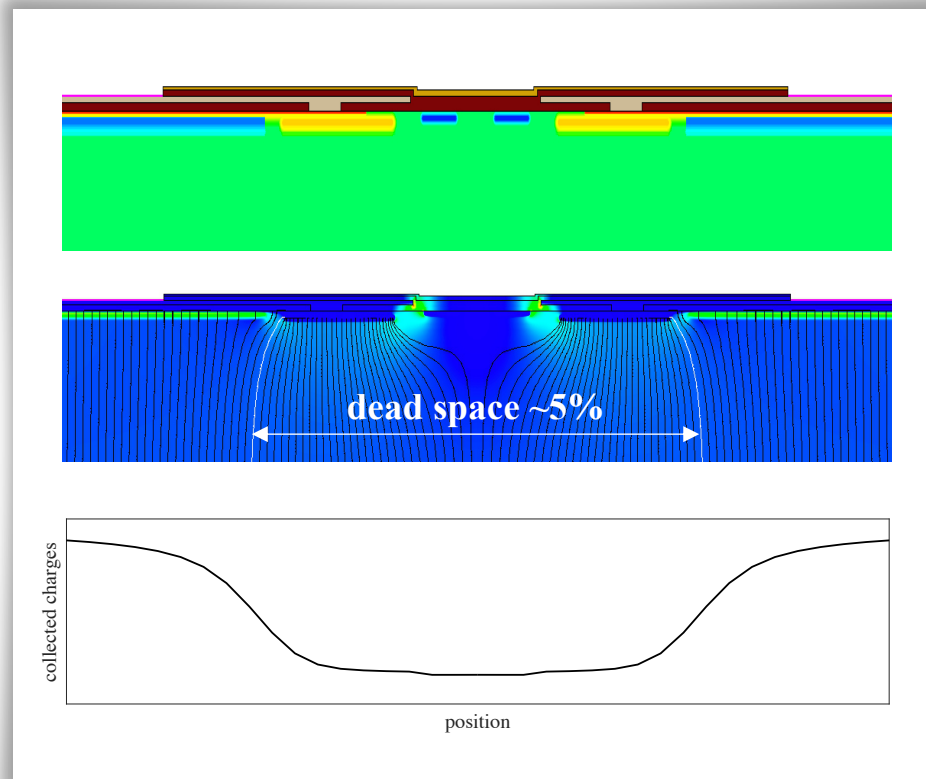
## 1. Study of detector static/dynamic characteristics: $I(V)$ , $G(V)$ , $C(V)$ , ...



$$\alpha_{n,p}(\mathcal{E}) = \gamma A_{n,p} \exp\left(-\gamma \frac{B_{n,p}}{\mathcal{E}}\right)$$

# Design and simulation of LGAD

## 2. Analysis about the internal **electric fields**: efficiency issues, ...

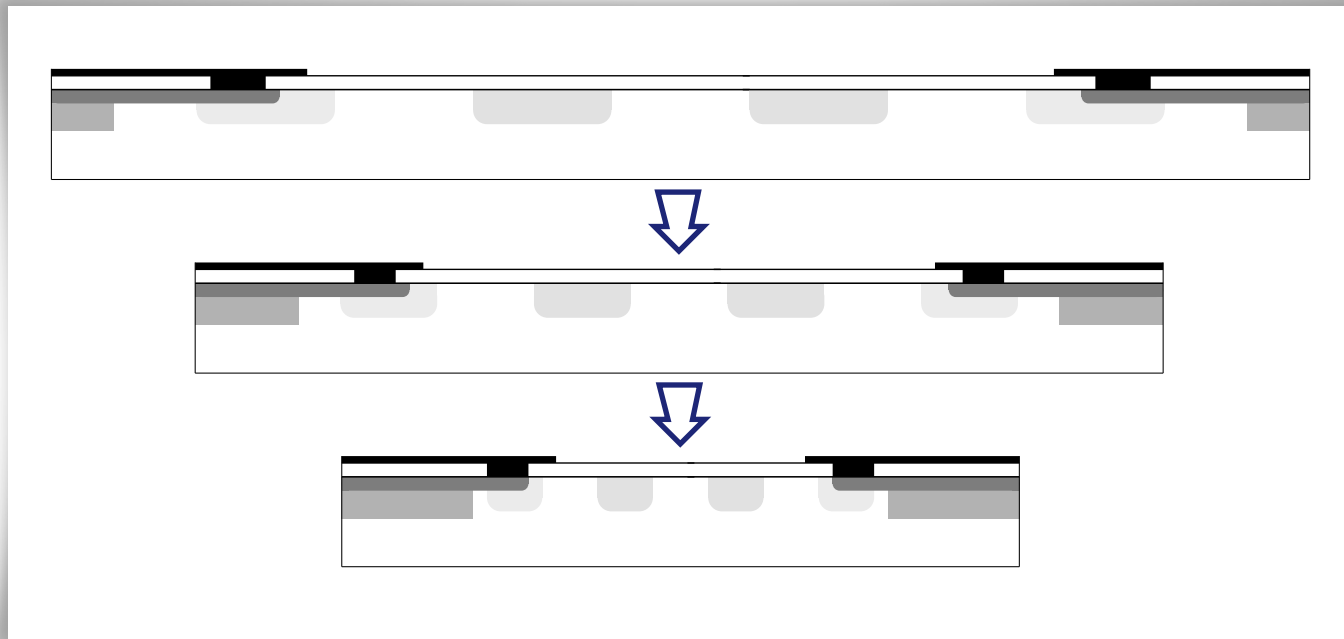


# Design and simulation of LGAD

2. Analysis about the internal **electric fields**: efficiency issues, ...

- **Two main strategies:**

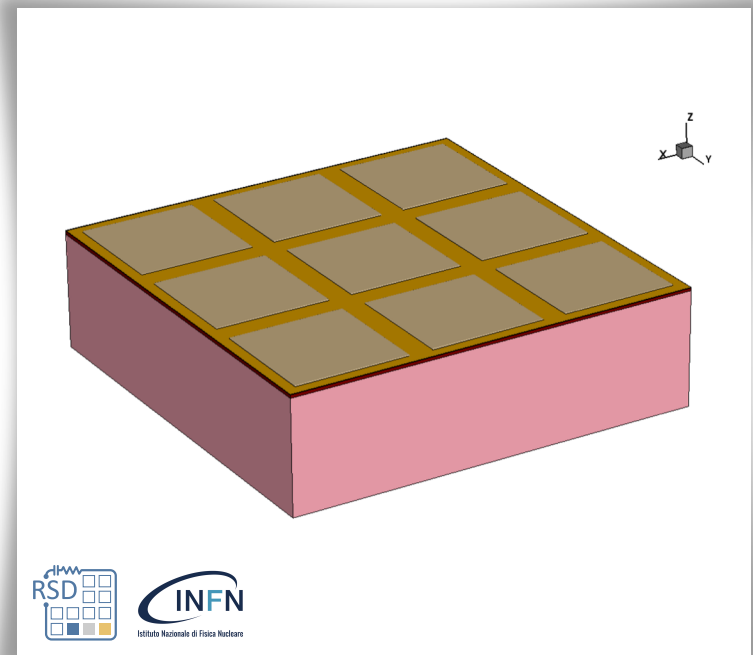
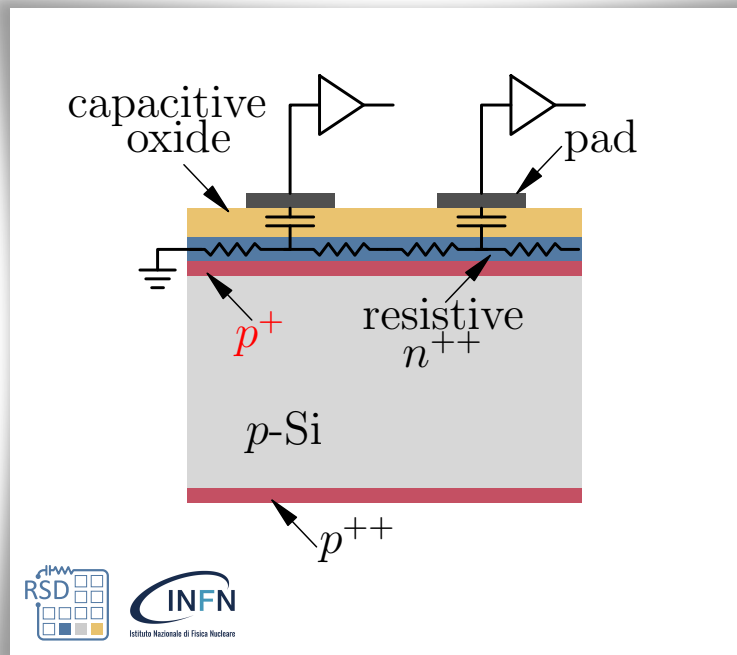
- a. layout scaling*



# Design and simulation of LGAD

## 2. Analysis about the internal **electric fields**: efficiency issues, ...

- **Two main strategies:**
  - b. implement a new readout approach*



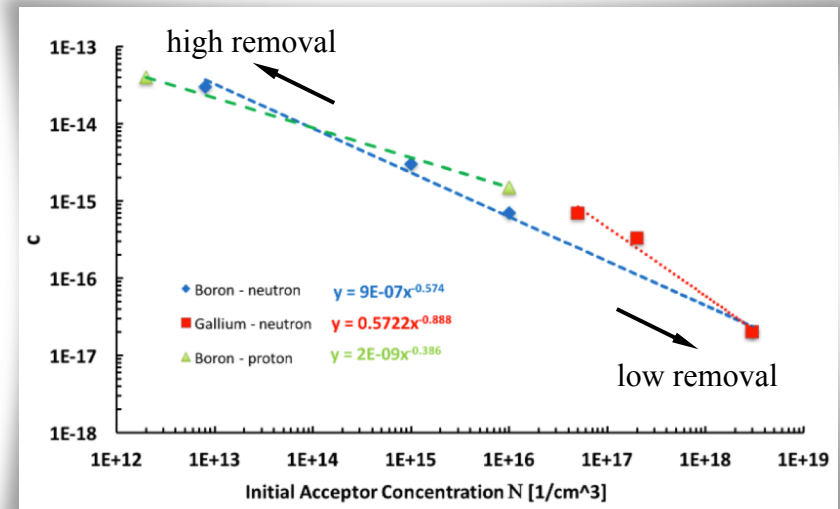
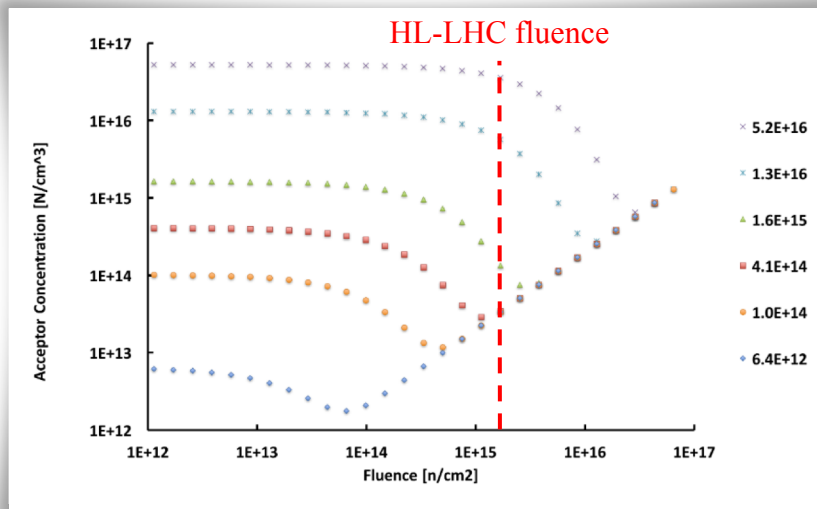
# Design and simulation of LGAD

## 3. Radiation tolerance

empirical acceptor removal/creation law

$$N_A(\phi, x) = g_{\text{eff}} \phi + N_A(0, x) e^{-c(N_A(0, x))\phi}$$

$$c(N_A(0, x)) = \alpha N_A(0, x)^{-\beta}$$





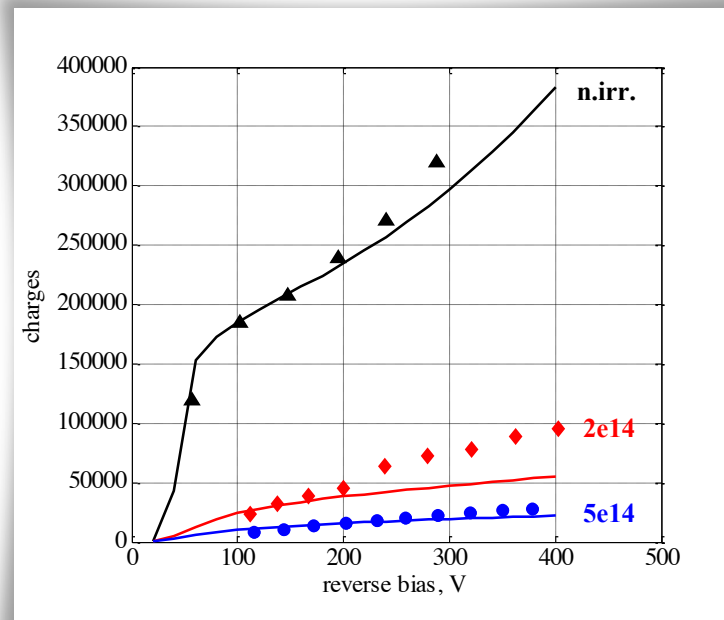
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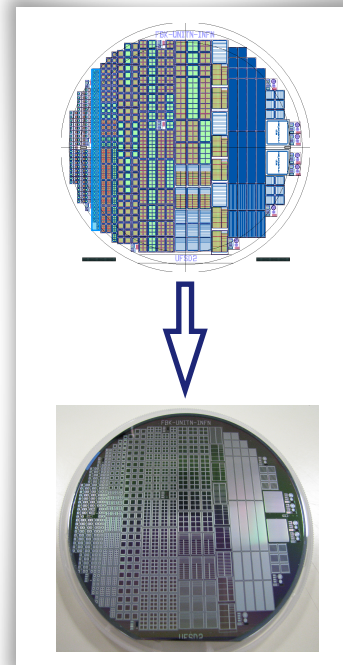
# Design and simulation of LGAD

1. Study of detector **static/dynamic characteristics**:  $I(V)$ ,  $G(V)$ ,  $C(V)$ , ...
- +
2. Analysis about the internal **electric fields**: efficiency issues, ...
- +
3. **Radiation tolerance**

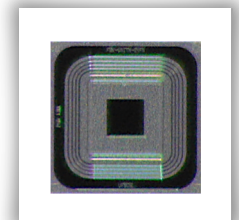
1. + 3.  
➔

Wafer #	Dopant	Gain dose	Carbon
1	Boron	0.98	
2	Boron	1.00	
3	Boron	1.00	
4	Boron	1.00	low
5	Boron	1.00	High
6	Boron	1.02	low
7	Boron	1.02	High
8	Boron	1.02	
9	Boron	1.02	
10	Boron	1.04	
11	Gallium	1.00	
14	Gallium	1.04	
15	Gallium	1.04	low
16	Gallium	1.04	High
18	Gallium	1.08	

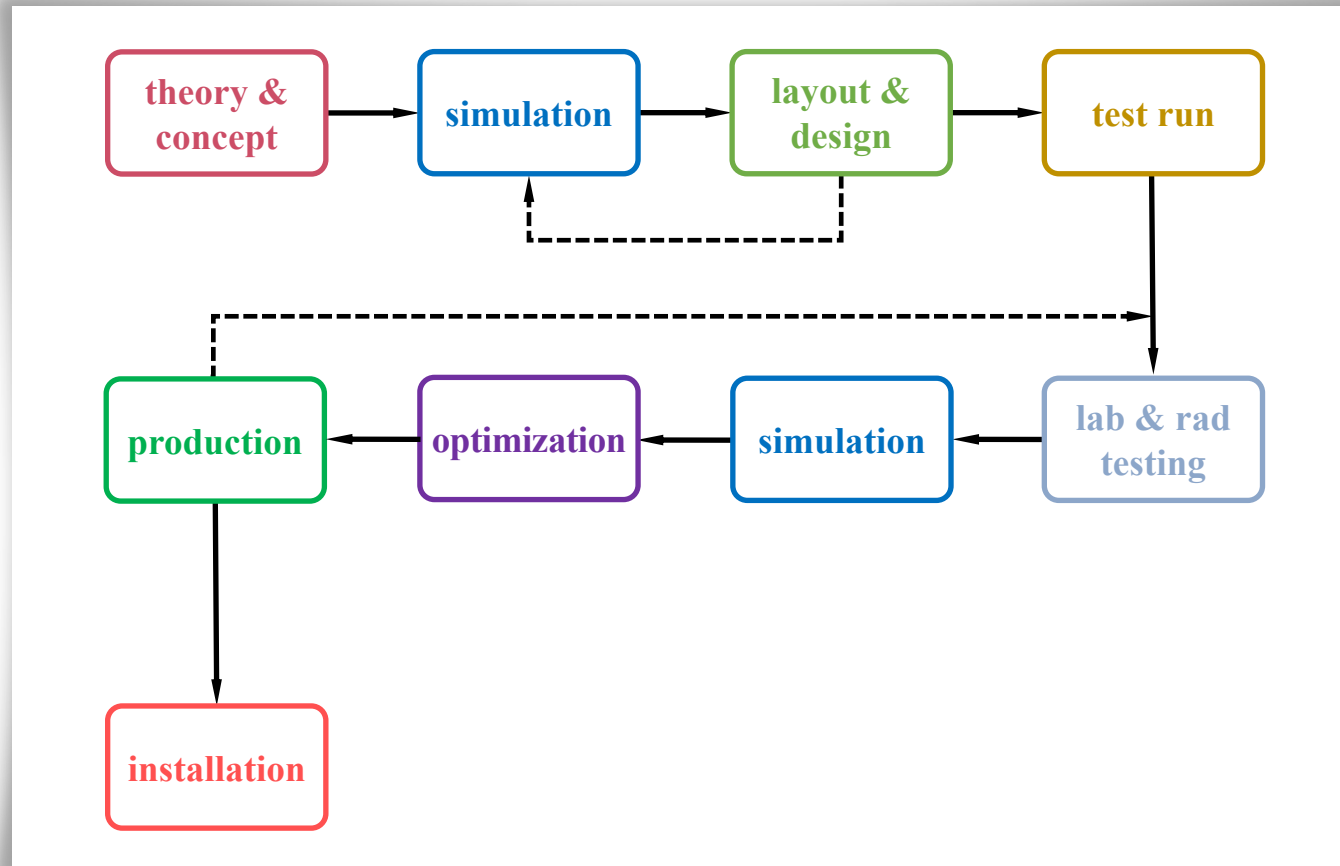
2.  
➔



➔



# LGAD production: the complete workflow!

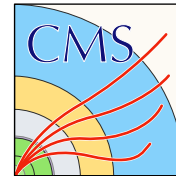
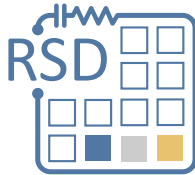


# Contacts and Info

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